



Onboard Trajectory Planning for a New Class of Hybrid Aircraft

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Outline

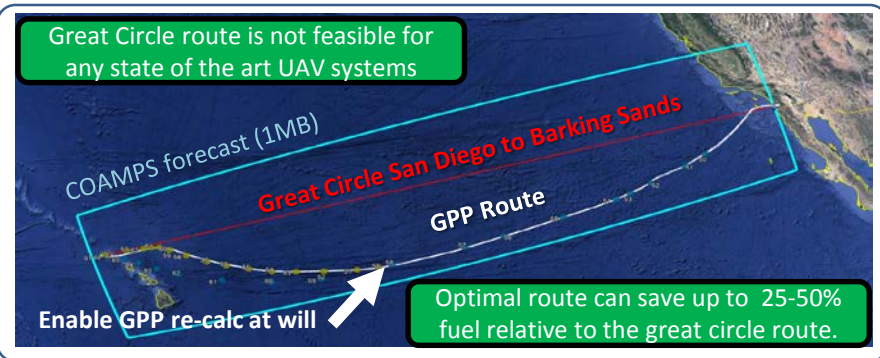
- Motivation – energy efficiency
- Approach:
 - *intelligent control
 - a/c design & new instrumentation & novel propulsion
- OC task formulation & control synthesis
- Results:
 - “Synthetic” weather
 - COAMPS weather
- Computational bottlenecks:
 - Existing solutions
 - Desired but Missing “pieces”
- What is achievable today



Motivation – “Multi-Day Endurance of a Group 2 UAS Utilizing Pacific Energy Sources”



Motivation – enhance current mission effectiveness via advanced energy behavior (DOD Operational Energy)



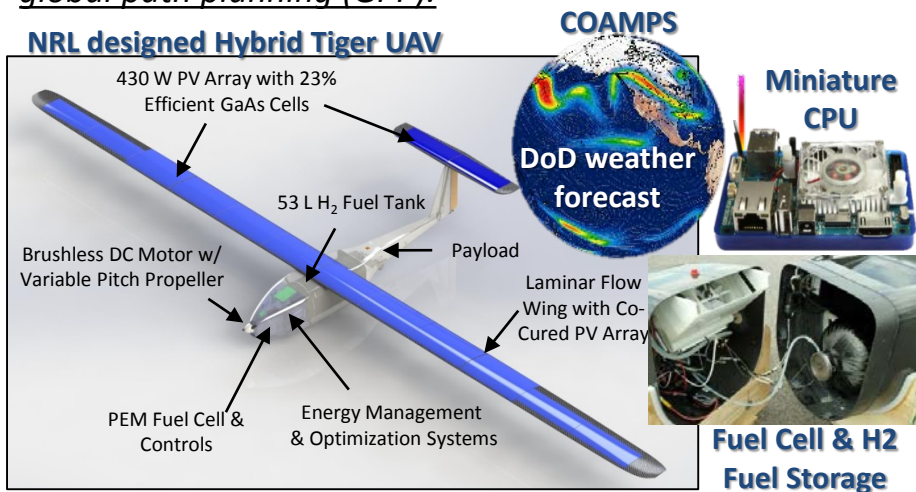
Objective – advance operational energy strategy:

- Increase future UAV capability via adaptable use of various sources of energy
- Enhance current mission effectiveness via predictive energy forecast and optimal routing
- Identify and reduce risk of energy shortage via robust adaptive mission replanning and intelligent control

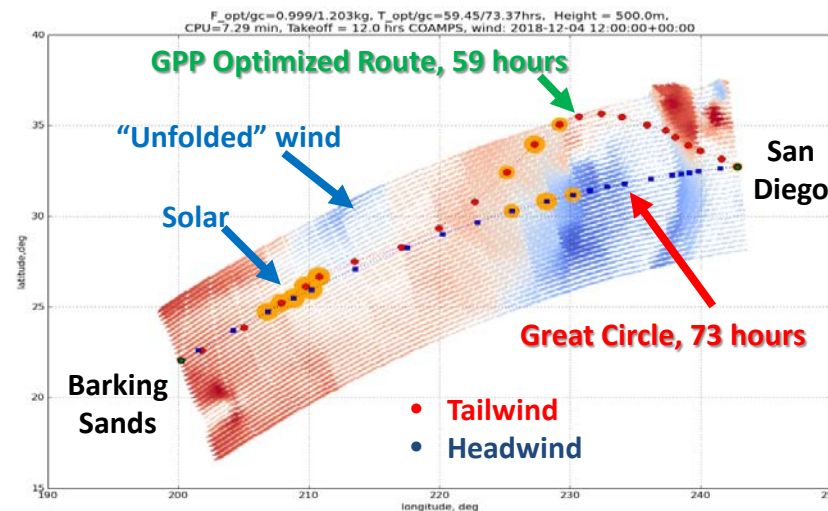
Concept – demonstrate synergistic range and endurance benefits by integrating fuel cell propulsion, soaring, solar harvesting, and optimal path planning.

Approach – integrate the latest advances in energy storage, harvesting, and recovery technologies in the novel onboard software capable of rapid *energy optimal global path planning (GPP)*.

NRL designed Hybrid Tiger UAV



Solution – minimum energy/fuel solution obtained by utilizing classical Pontryagin optimal control approach. **Key Deliverable** - previously not feasible routes (CA-HI) can be optimally flown and rapidly recomputed onboard.



Patent: U.S. PTO 16/155,968, U.S. PCT PCT/US18/55144

Existing Constraints & Desired Features

Desired features of the GPP solution:

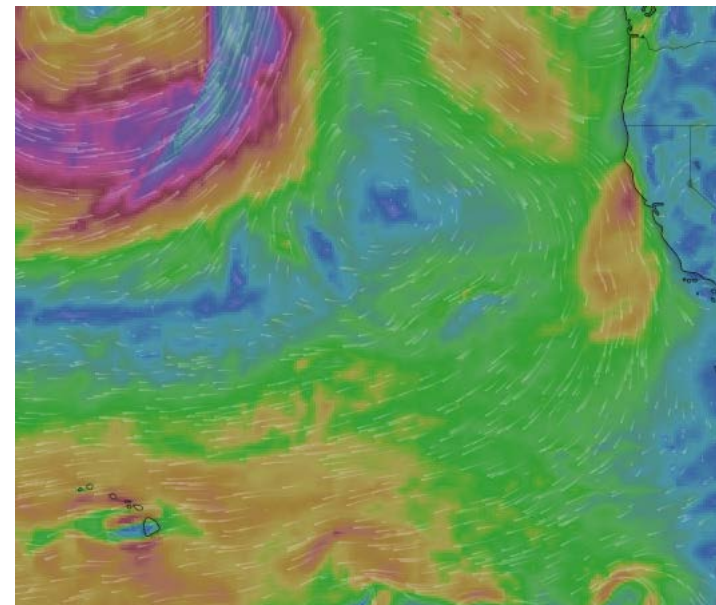
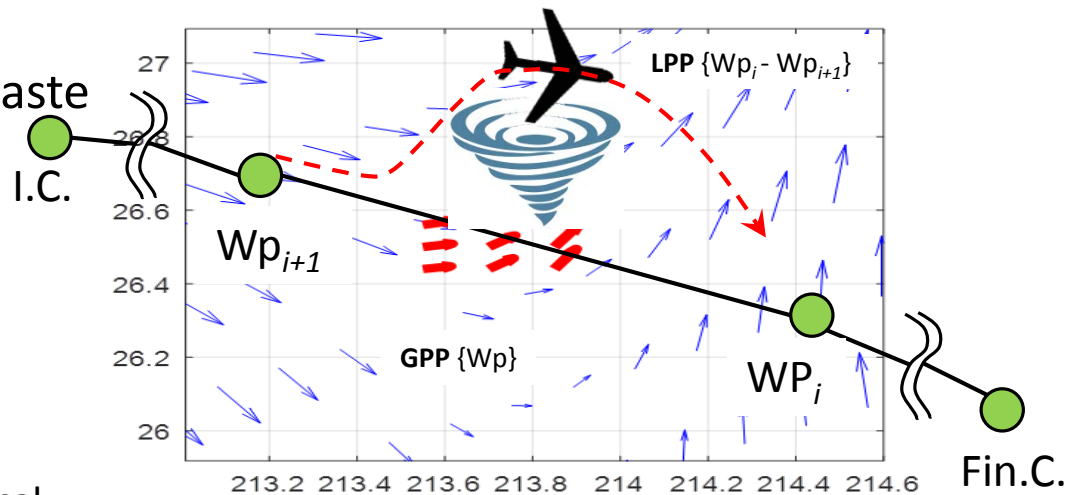
- Completeness - need guarantees of complete exploration of given domain
- Optimality – need analytical guarantees of optimality of the solution
- Feasibility – practically feasible to implement onboard
 - feasibility of CPU load
 - feasibility of memory allocation
 - ability to monitor the solver as it runs

Constraints of many of the existing methods:

- NO closed-form solution for complex dynamics of aircraft
 - FAIL in complex and dynamic environment (time-varying wind, obstacles, etc)
 - INFEASIBLE for online onboard implementation
 - LACK of convergence for stiff ODEs
 - Initial guess - problematic
-
- "SURVEY OF NUMERICAL METHODS FOR TRAJECTORY OPTIMIZATION," by John Betts, Journal of Guidance, Control, and Dynamics, vol. 21, #2, March-April 1998.
 - "OPTIMAL CONTROL AND NUMERICAL SOFTWARE: AN OVERVIEW" by H.S. Rodrigues, M.T. Monteiro, D.M. Torres, in 'Systems Theory: Perspectives, Applications and Developments', Nova Science Publishers, Editor: Francisco Miranda, Jan 2014.
 - "A SURVEY OF NUMERICAL METHODS FOR OPTIMAL CONTROL" by Anil V. Rao, AAS 09-334
 - "OPTIMAL PATH PLANNING AND POWER ALLOCATION FOR LONG ENDURANCE SOLAR-POWERED UAV," by S.Hosseini, R.Dai, M. Mesbahi, in proceedings of ACC2013, Washington, DC, June 17-19, 2013

Mission Planning

- Practical objective – maximum endurance by minimizing the waste of constrained energy resource onboard
- Challenges:
 - Weather:
 - time-varying weather = {wind, local thermals, solar irradiance}
 - stochastic nature diverging with time
 - limited fidelity
 - Limited communication and computational resources
- Approach:
 - Global route – GPP
 - Local route – LPP
 - GPP is a “reference to follow” for the LPP



Key Components of GPP

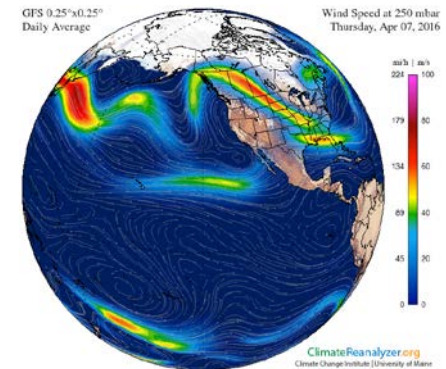
• Aircraft

- Aerodynamics C_L , C_D
- Fuel consumption dynamics vs thrust
- Solar efficiency
- “Battery” efficiency (minor now, big potential)



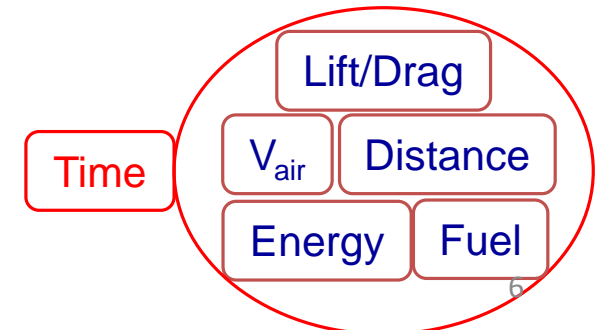
• Weather prediction model – COAMPS NRL/MRY

- 3D wind components as functions of LLA & Time
- Solar flux => essential chunk of energy
- PBL => essential chunk of hybrid power
- Variability of weather => confidence



• Time

- Defines non-autonomous nature
- Optimizes the entire mission => start of the mission
- “Convolution parameter” of Energy&Dynamics of flight



Plant Model

- Aircraft :

$$\dot{x} = V \cos \psi + W_x(x, y, t)$$

$$\dot{y} = V \sin \psi + W_y(x, y, t)$$

$$\dot{\psi} = \frac{g \tan \varphi}{V_g}; V_g = \sqrt{\dot{x}^2 + \dot{y}^2}$$

$$u_1 = \varphi(t) - \text{bank angle}$$

$$u_2 = V(t) - \text{airspeed}$$

- Power loss due to drag

$$C_L = \frac{2W}{\rho V^2 S \cos \varphi}$$

$$C_D = C_{D_0} + K \cdot C_L^2$$

$$D = \frac{\rho V^2}{2} S \cdot C_D$$

$$T = D$$

$$P_{drag} = \frac{T \cdot V}{\eta_{prop}}$$

$$E_{drag} = \int_0^{t_f} P_{drag}(\varphi, V, t) dt$$

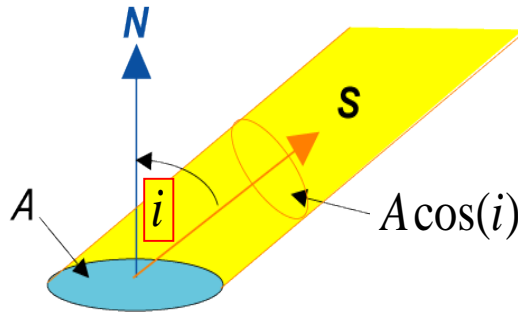
- Separating controls (φ and V) from the parameterized model

$$P_{drag} = \frac{T \cdot V}{\eta_{prop}} = \frac{\rho V^3}{2\eta_{prop}} S \cdot (C_{D_0} + K_p \cdot C_L^2) =$$

$$= \frac{\rho V^3}{2\eta_{prop}} S \cdot C_{D_0} + \frac{\rho V^3}{2\eta_{prop}} S \cdot K_p \cdot C_L^2 = \frac{\rho V^3}{2\eta_{prop}} S \cdot C_{D_0} + \frac{\rho V^3}{2\eta_{prop}} S \cdot K_p \cdot \frac{4W^2}{\rho^2 V^4 S^2 \cos^2 \varphi} =$$

$$= \frac{\rho \cdot S \cdot C_{D_0}}{2\eta_{prop}} \cdot V^3 + 2 \frac{K_p S \left(\frac{W}{S}\right)^2}{\rho \eta_{prop}} \cdot \frac{1}{V \cos^2 \varphi} = K_{p1} \cdot V^3 + K_{p2} \cdot \frac{1}{V \cos^2 \varphi}$$

Plant Model



- Power gain due to solar photovoltaics

$$\cos(i) = \cos(\varphi) \sin(El) - \cos(E) \sin(Az - \psi) \sin(\varphi)$$

$Az(t), El(t)$ – azimuth and elevation of Sun

$$P_{solar} = \eta_{solar} P_{sflux} A_{PV} \cos(i)$$

$$E_{solar} = \int_{t_{start}}^{t_f} P_{solar}(\varphi, V, t) dt$$

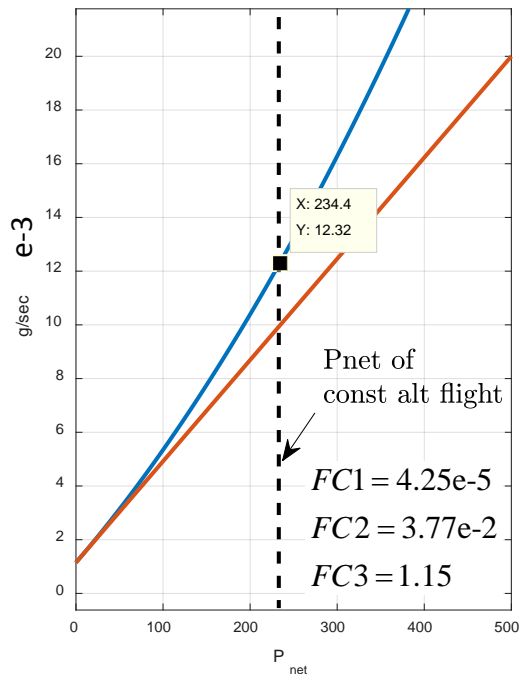
- Fuel consumption model

$$P_{net}(\varphi, V, t) = |P_{drag} - P_{solar}|$$

$$\dot{m}_F = FC1 \cdot P_{net}^2 + FC2 \cdot P_{net} + FC3$$

$$m_F = \int_{t_{start}}^{t_f} \dot{m}_F(\varphi, V, t) dt$$

$\delta = 0.2e-3 \Rightarrow \varepsilon = 172 \text{ g over 24 hours}$
 period \Rightarrow 17 hours of flight; $\sim 10 \text{ g/hour}$

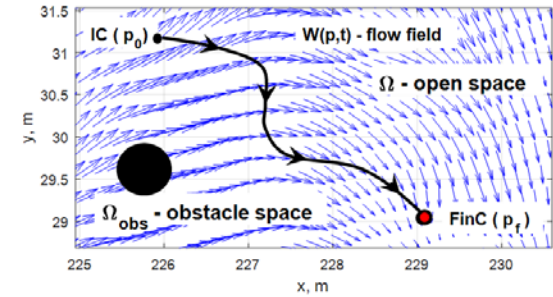


Minimum Energy Optimum Control

Find the optimal airspeed V^* and bank angle φ^* control functions that minimize

$$J^* = \min_{\varphi^*, V^*} \int_{t_0}^{t_f} P_{net} dt$$

subject to the states and costates dynamics



$$\dot{x} = V \cos(\psi) + W_x(x, y, t)$$

$$\dot{y} = V \sin(\psi) + W_y(x, y, t)$$

$$\dot{\psi} = g \tan(\varphi) / V_g, V_g = \sqrt{\dot{x}^2 + \dot{y}^2}$$

$$\dot{\tau} = 1, \tau = t/t_f$$

, where

$$\dot{\lambda}_x = -\partial H / \partial x = -\lambda_x \frac{\partial W_x(x, y, t)}{\partial x} - \lambda_y \frac{\partial W_y(x, y, t)}{\partial x} - \lambda_\psi \frac{\partial \dot{\psi}}{\partial x}$$

$$\dot{\lambda}_y = -\frac{\partial H}{\partial y} = -\lambda_x \frac{\partial W_x(x, y, t)}{\partial y} - \lambda_y \frac{\partial W_y(x, y, t)}{\partial y} - \lambda_\psi \frac{\partial \dot{\psi}}{\partial y}$$

$$\dot{\lambda}_\psi = -\frac{\partial H}{\partial \psi} = \lambda_x V \sin(\psi) - \lambda_y V \cos(\psi) + K_s \sin(\phi) \cos(e) \cos(a - \psi) - \lambda_\tau \frac{\partial \dot{\psi}}{\partial \psi}$$

$$\dot{\lambda}_\tau = -\frac{\partial H}{\partial \tau} = -\lambda_x \frac{\partial W_x(x, y, t)}{\partial \tau} - \lambda_y \frac{\partial W_y(x, y, t)}{\partial \tau} - \lambda_\psi \frac{\partial \dot{\psi}}{\partial \tau}$$

$$H = V^3 K_{p1} + K_{p2} / V \cos^2(\varphi) - K_s \cos(\theta_i) + \lambda_x \dot{x} + \lambda_y \dot{y} + \lambda_\psi \dot{\psi} + \lambda_\tau$$

and the associated boundary conditions

$$x(t_0) = x_0; y(t_0) = y_0$$

$$x(t_f) = x_f; y(t_f) = y_f$$

$$\psi(t_0) = \psi_0; \psi(t_f) = \psi_f$$

$$\tau(t_0) = 0; \tau(t_f) = 1$$

$$+ H(x, y, \psi, \tau, \lambda_x, \lambda_y, \lambda_\psi, \lambda_\tau)_{t_f} = 0$$

Synthesis

A1: Aircraft is equipped with a stabilizing autopilot that effectively eliminates the nonlinear flight dynamics from consideration.

A2: The bank angle φ is small.

$$\frac{\partial H}{\partial \varphi} = \frac{2K_{P2}}{V} \tan \varphi (\tan^2 \varphi + 1) + K_s \sin \varphi \left(\sin(e) + \frac{\cos(e) \sin(a - \psi)}{\tan \varphi} \right) + \lambda_\psi \frac{g}{V_g} \frac{1}{\cos^2 \varphi} = 0$$

$$\frac{\partial H}{\partial V} = 3V^2 K_{P1} - \frac{1}{V^2} K_{P2} (\tan^2 \varphi + 1) + \lambda_x \cos \psi + \lambda_y \sin \psi = 0$$

Results:

$$\tan(\varphi^*) = - \frac{V \lambda_\psi g + V_g K_s \cos(e) \sin(a - \psi)}{V_g (2K_{P2} + V \cdot K_s \sin(e))}$$

$$V^{*2} = \sqrt{\frac{4K}{3\rho^2 C_{D0}} \left(\frac{mg}{S} \right)^2} + \frac{\eta_{prop}}{18\rho S C_{D0}} \Lambda^2 - \frac{\eta_{prop}}{3\rho S C_{D0}} \Lambda$$

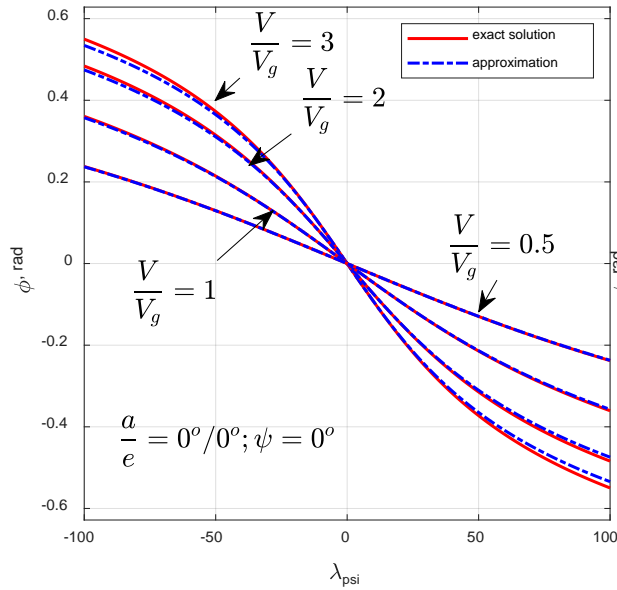
$$\Lambda = \lambda_x \cos \psi + \lambda_y \sin \psi$$

$$V_{minP}^2 = \frac{2mg}{\rho S} \sqrt{\frac{K}{3C_{D0}}}$$

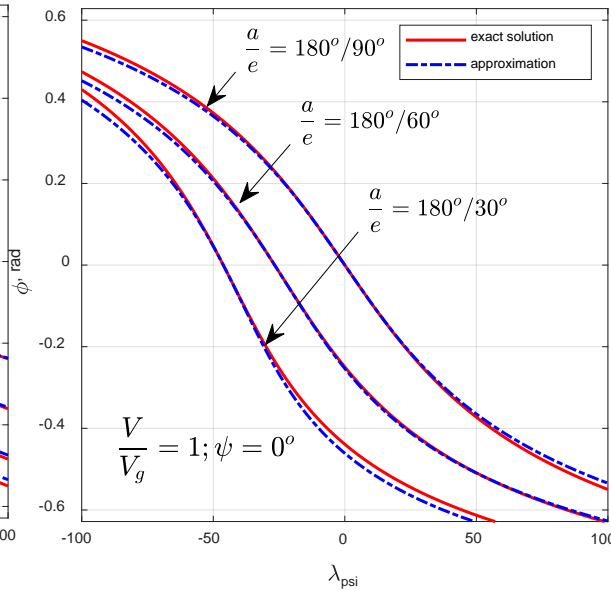
the optimal speed to fly for the minimum required power V_{minP} in horizontal flight

OC Analysis

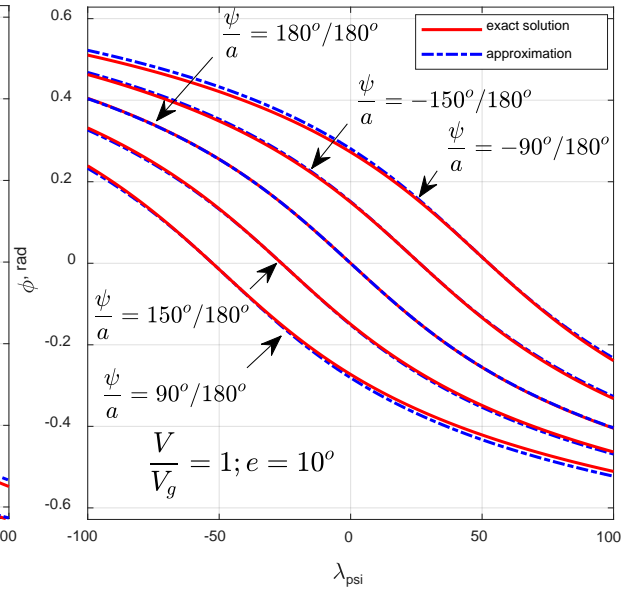
$$\tan(\varphi^*) = -\frac{V}{V_g} \frac{\lambda_\psi g + V_g K_s \cos(e) \sin(a - \psi)}{2K_{p2} + V \cdot K_s \sin(e)}$$



a. airspeed



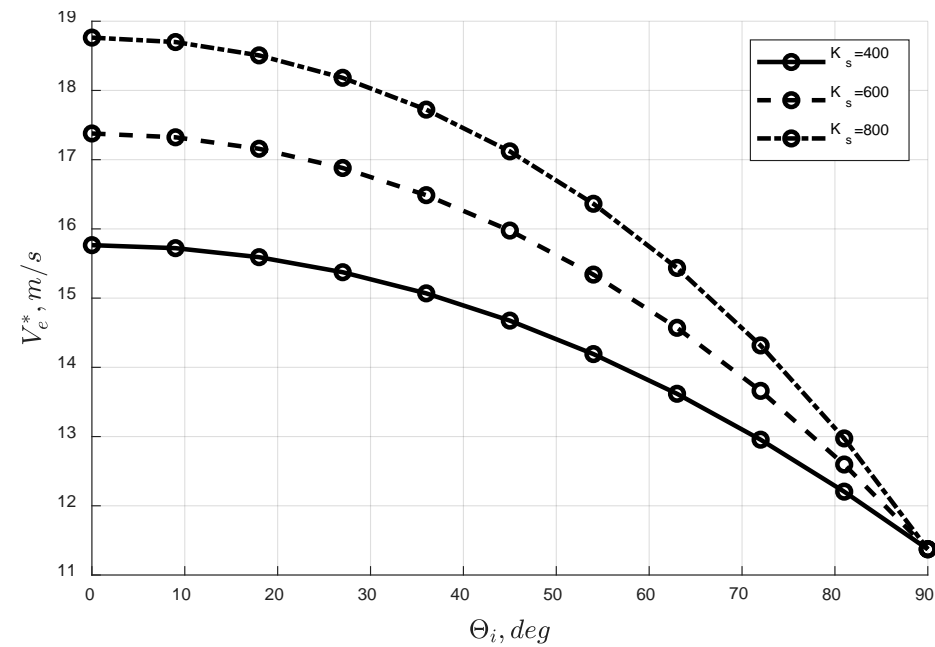
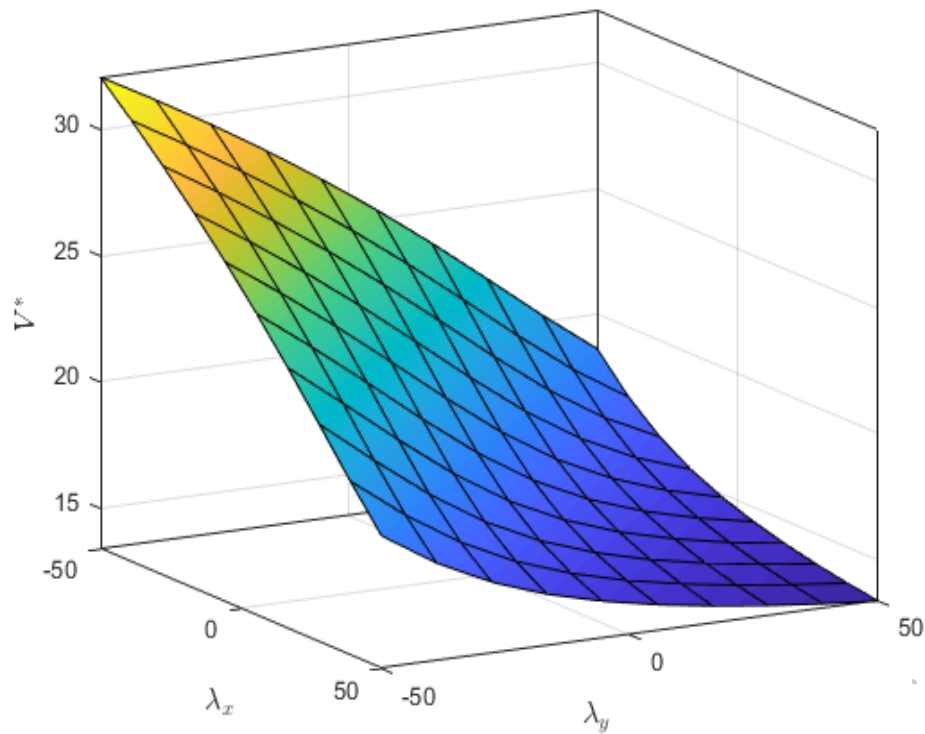
a. sun elevation



a. sun azimuth

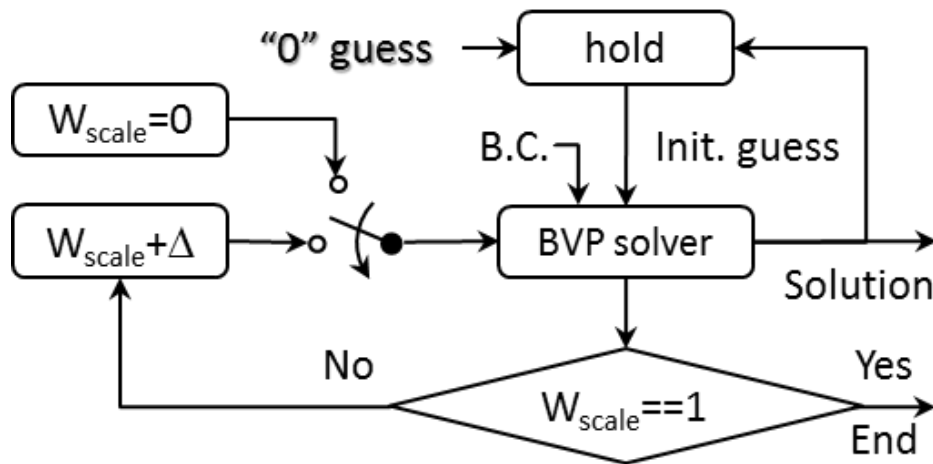
OC Analysis

$$V^{*2} = \sqrt{\frac{4K}{3\rho^2 C_{D0}} \left(\frac{mg}{S}\right)^2 + \frac{\eta_{prop}}{18\rho S C_{D0}} \Lambda^2 - \frac{\eta_{prop}}{3\rho S C_{D0}} \Lambda}$$

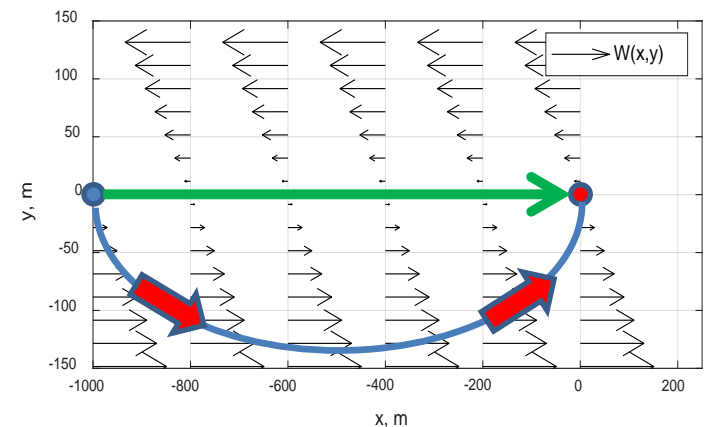


Solving BVP

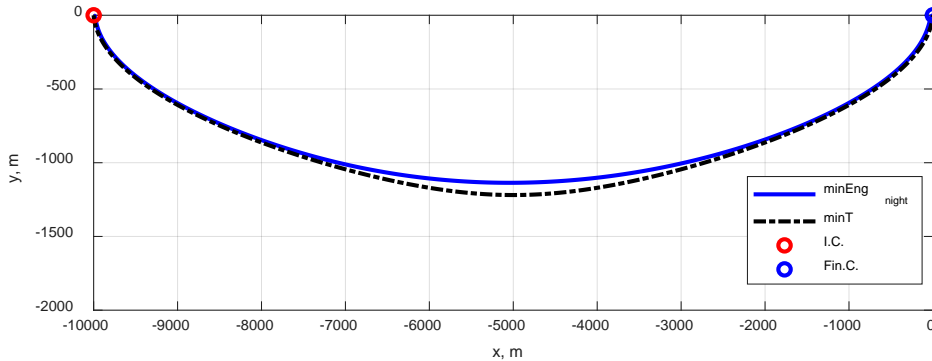
- Challenge - sensitivity to the initial guess:
 - Scaling
 - Continuation
 - Homotopy methods
- design and solve a sequence of problems starting with a trivial one, and then use the previous solution as an initial guess for the next one.
- Solution – when there is no wind $\Rightarrow W_{\text{scale}} = 0 \Rightarrow$ the resulting trajectory is necessarily a straight line



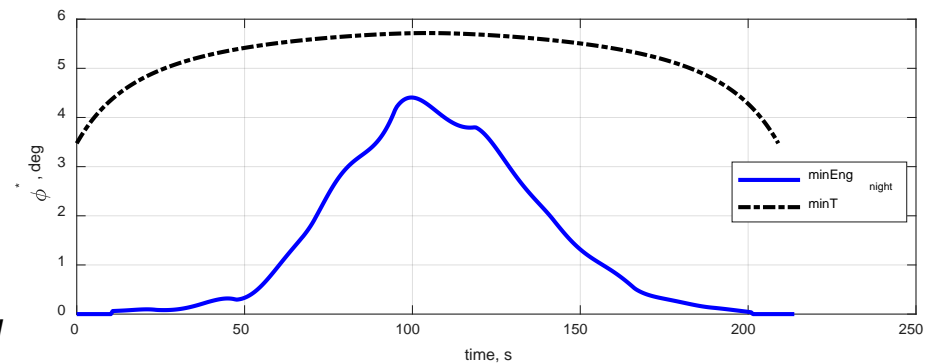
$$W_x(x, y, t) = -h_y \cdot y, W_y(x, y, t) = 0$$



Synthetic Wind :: Night

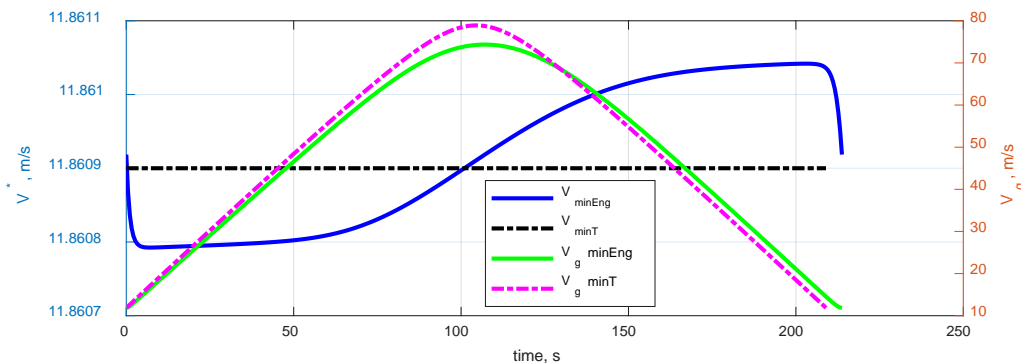


a – trajectories



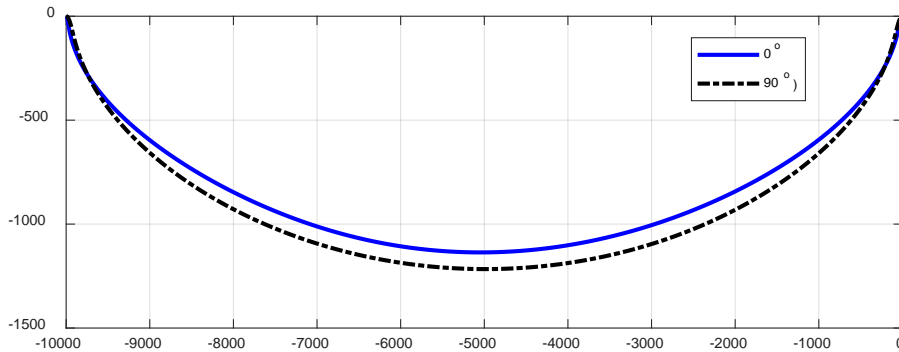
b – ϕ control

c – the airspeed V and the ground speed V_g

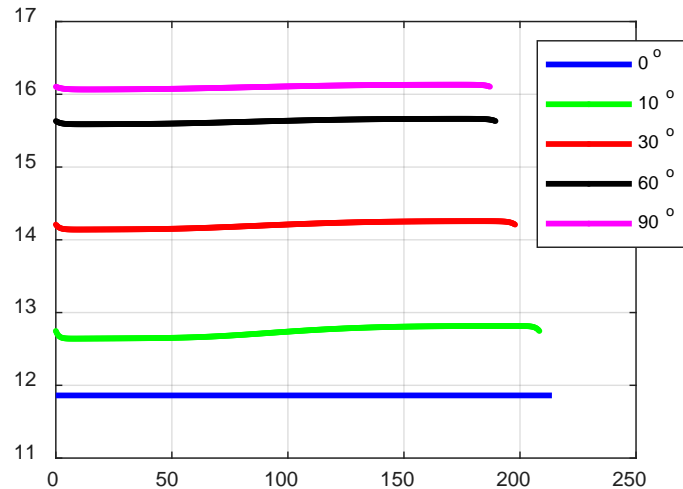


- Synthesized OC closely approximates *minT* solution of Zermelo task
- BVP solver is fast => seconds

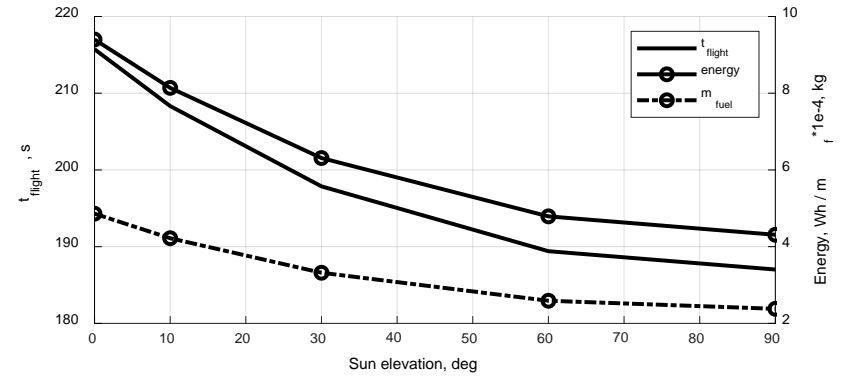
Synthetic Wind :: Day



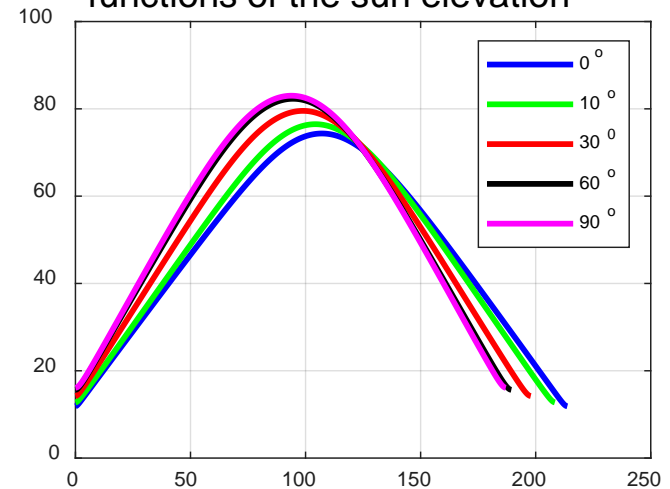
a – trajectories



b – the airspeed



d - Energy and flight time as functions of the sun elevation

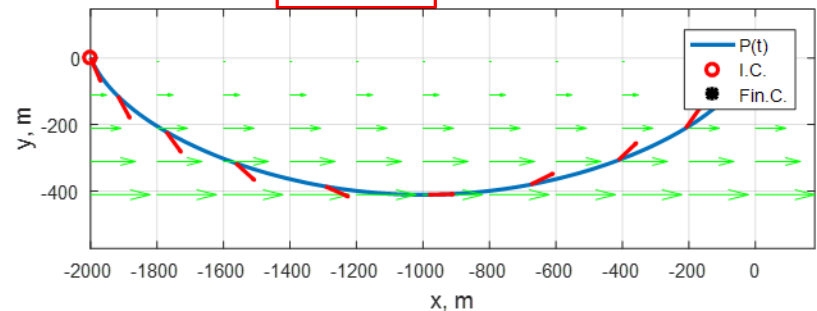


c – the ground airspeed V_g

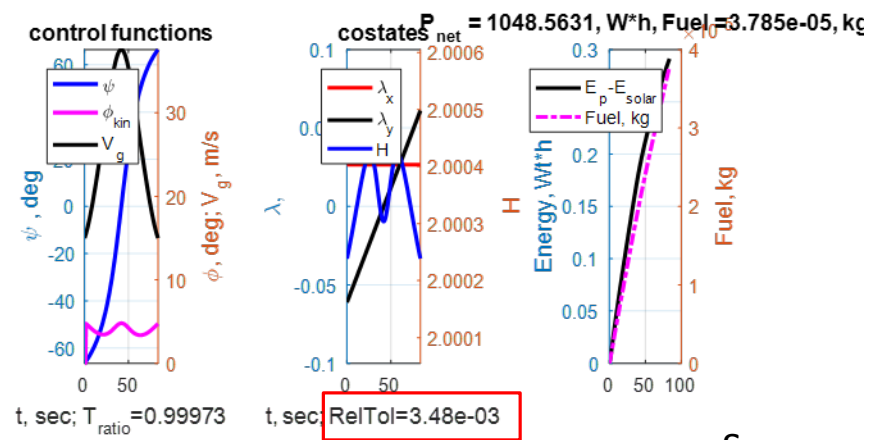
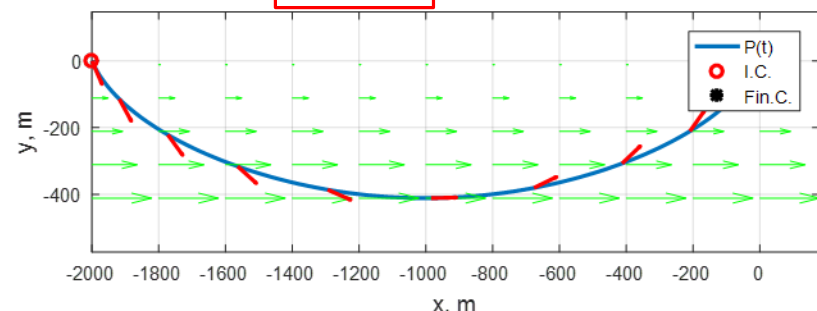
- Synthesized OC is sufficiently different however can be 'initialized' by $minT$

CPU time reduced by ~4.7 times

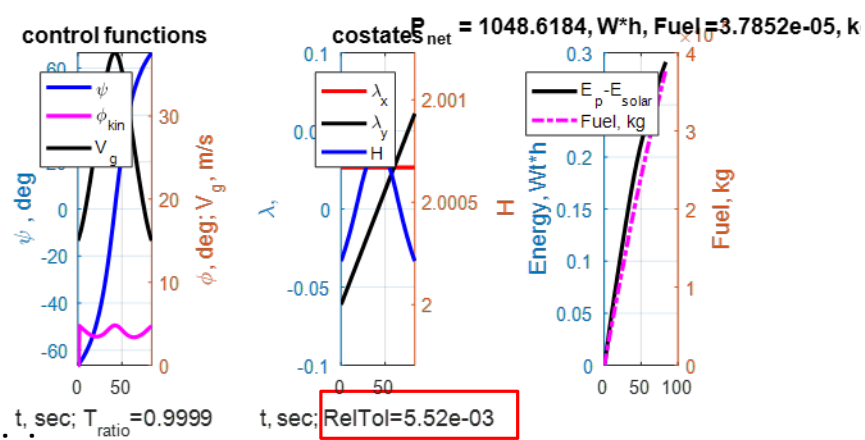
minTime = 83.5805 sec, **CPU = 73.2379**, Solar Az/Elev = 0/70, Vw/h=2.2/40, $V_a = 15$



minTime = 83.5838 sec, **CPU = 15.5172**, Solar Az/Elev = 0/70, Vw/h=2.2/40, $V_a = 15$



Single shot

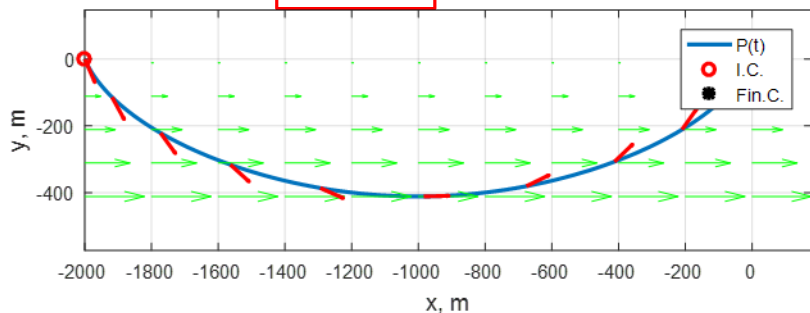


Continuation

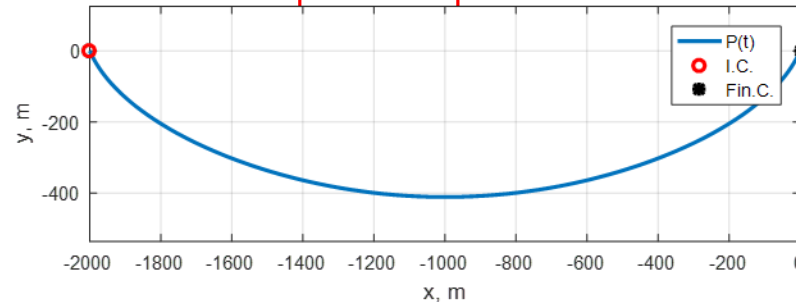
Same precision

CPU time reduced by 26 times

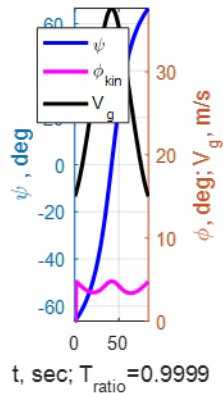
minTime = 83.5838 sec, **CPU = 15.5172**, Solar Az/Elev = 0/70, Vw/h=2.2/40, $V_a=15$



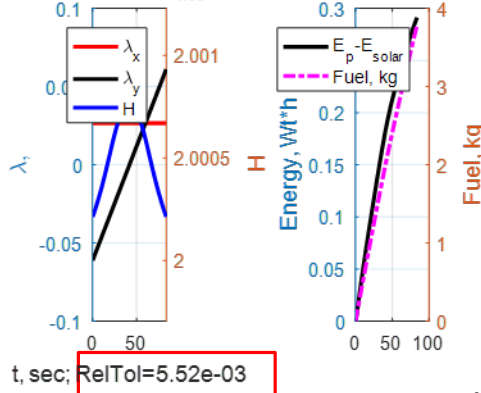
minTimeScaled = 83.5978 sec, **CPU = 0.57562**, Solar Az/Elev = 0/70, Vw/h=2.2/40, $V_a=1$



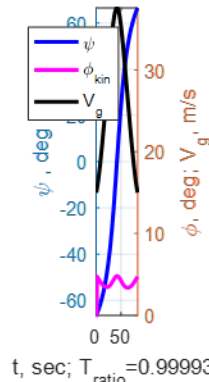
control functions



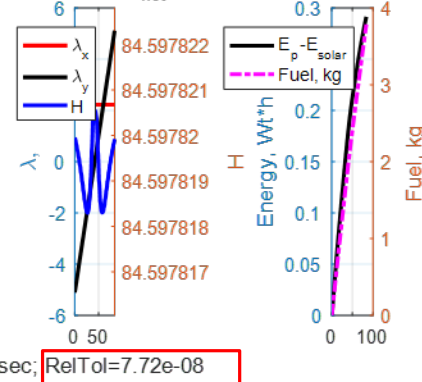
costates $P_{net} = 1048.6184$, W^*h , Fuel = $3.7852e-05$, kg



control functions



costates $P_{net} = 1048.7711$, W^*h , Fuel = $3.7858e-05$, kg



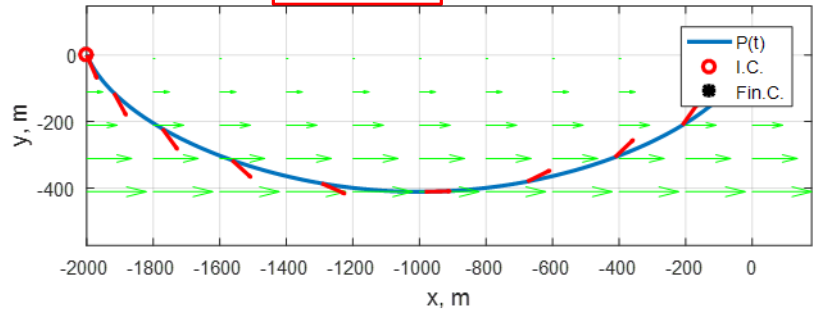
Improve precision

Continuation

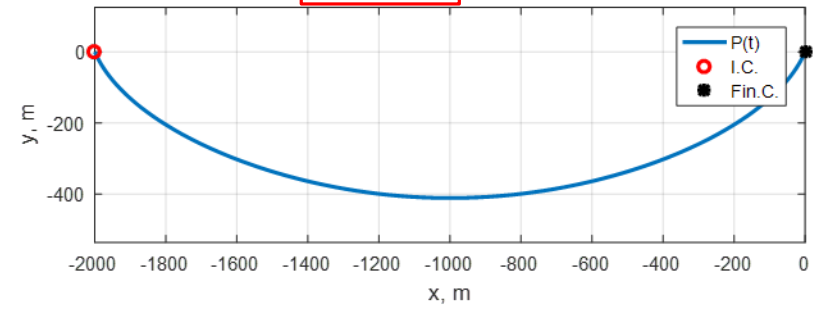
Continuation+Scaling

CPU time reduced by 127 times

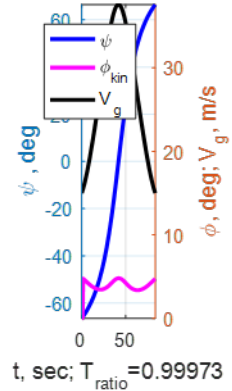
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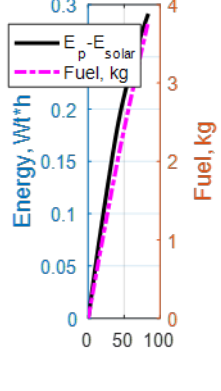
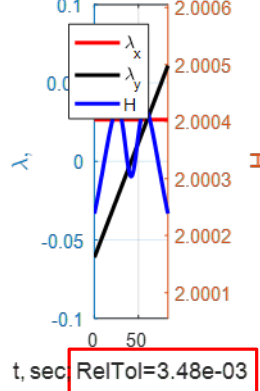
minTimeScaled = 83.5978 sec, **CPU = 0.57562**, Solar Az/Elev = 0/70, Vw/h=2.2/40, $V_a = 1$



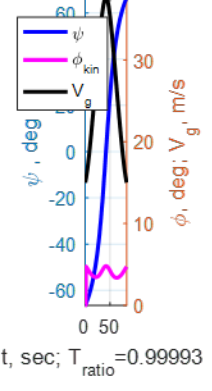
control functions



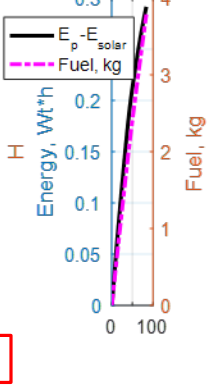
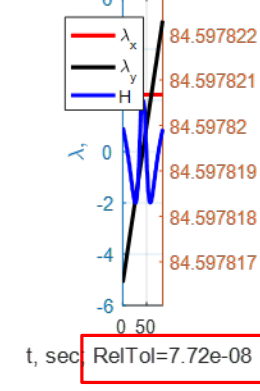
costates $P_{net} = 1048.5631$, W^*h , Fuel = $3.785e-05$, kg



control functions



costates $P_{net} = 1048.7711$, W^*h , Fuel = $3.7858e-05$, kg



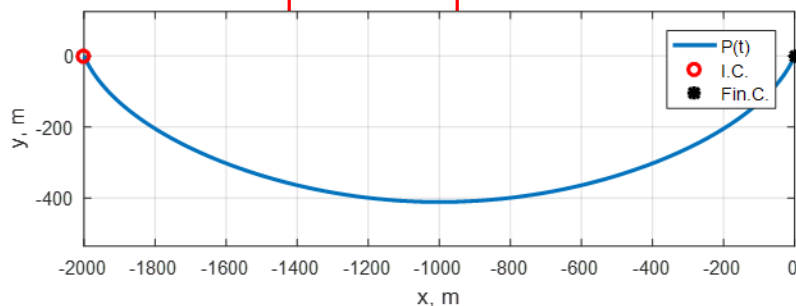
Improve precision

Single shot

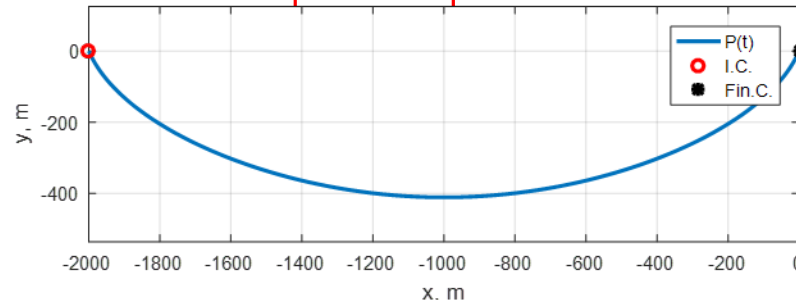
Continuation +Scaling

CPU time is ~2 times less

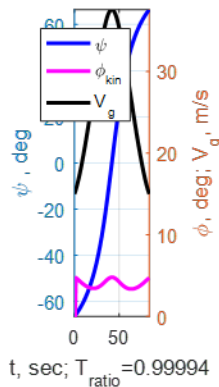
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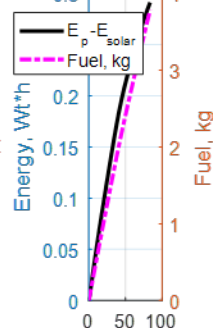
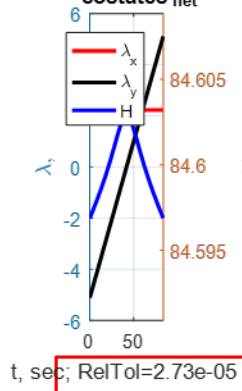
minTimeScaled = 83.5978 sec, CPU = 0.57562, Solar Az/Elev = 0/70, Vw/h=2.2/40, $V_a=1$



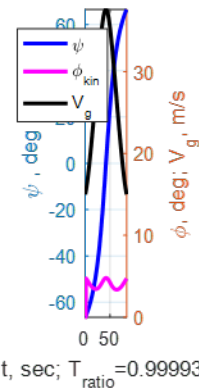
control functions



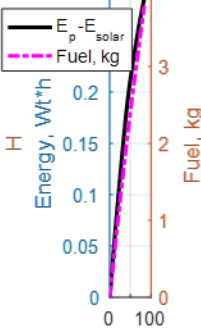
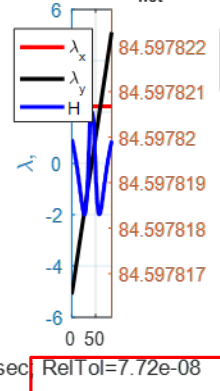
costates $P_{net} = 1048.7646$, W^*h , Fuel = $3.7857e-05$, kg



control functions



costates $P_{net} = 1048.7711$, W^*h , Fuel = $3.7858e-05$, kg



Precision is the price,
however "1e-3" is more than enough

Continuation +Scaling

Continuation +Scaling

Discretization = 100, the same for both methods

NOTE – keep in mind that there is **NO interpolation**

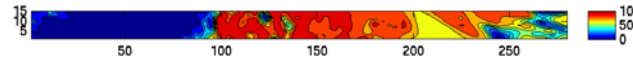
- **Continuation**:
 - improves convergence properties of bvp solver by parameterizing the task when a single shot solution is not guaranteed.
 - significantly simplifies the choice of an initial guess of states and co-states of the dynamic system.
 - reduces the computational time by a factor of $\sim \underline{5}$.
- **Scaling** of ODE
 - Reduces sensitivity of the BVP solver to nonlinearities.
 - Reduces the computational time by a factor of $\sim \underline{20}$.
- **Combination** of ODE Scaling and Continuation:
 - Combines the benefits of both.
 - Reduces computational time by more than a factor of $\sim \underline{100}$.
- What is **next**:
 - Use Scaling+Continuation result of minTime task as an initial guess of minEnergy & minFuel. Already prototyped with good promise.
 - Solve the GPP task with interpolated COAMPS data.

COAMPS Wind

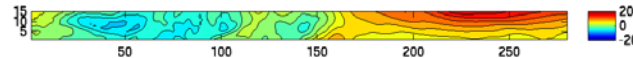
PBL Height



Relative Humidity 1.5 km ASL

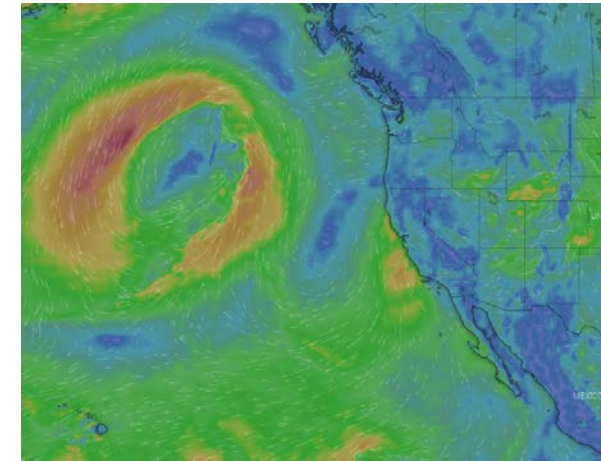


Zonal Wind 3 km ASL



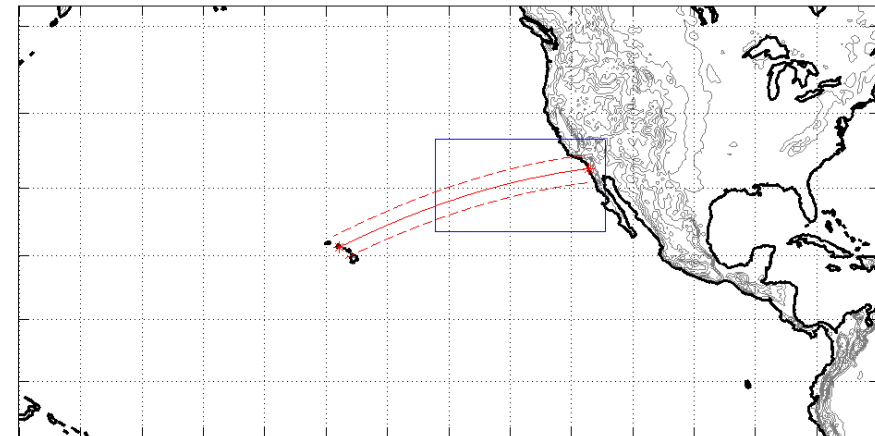
- Height levels: zonal, meridional, vertical winds, relative humidity
- Single levels: PBL height, incoming solar radiation, theta star (buoyancy measure)

70Mb/72hour



Solid red line -- great circle from SND-HNL

- Dashed lines represent a path ~200 km on each side of great circle.
- Path width is adjustable
- COAMPS data interpolated to regular grid along the path



Fast interpolation of vectorized queries is one of the heaviest computational tasks.

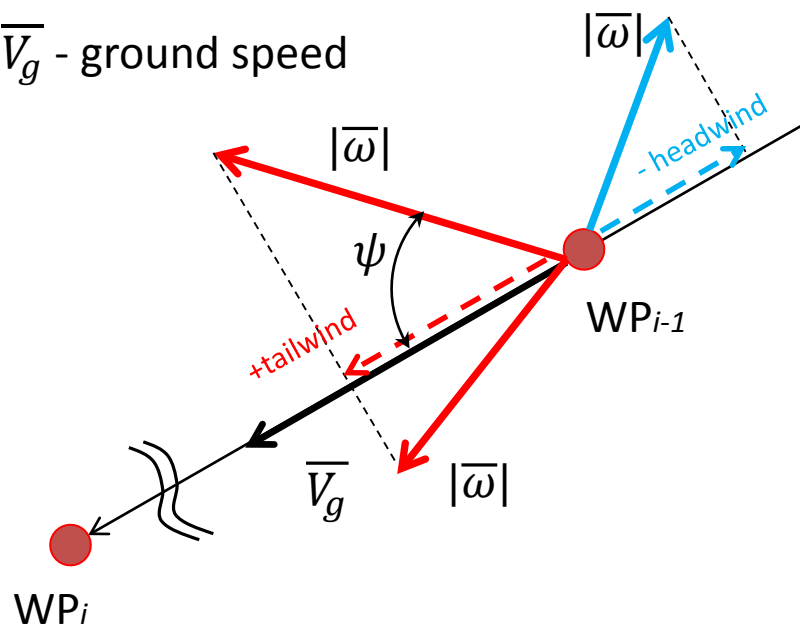
Interpretation of COAMPS-based results

Color-coding should capture:

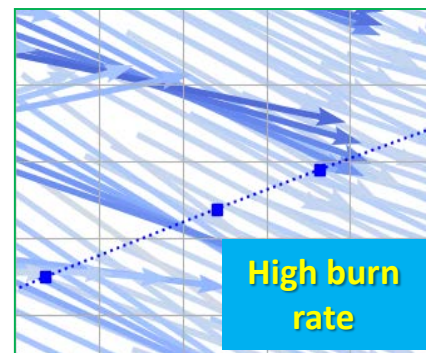
- Magnitude of wind
- Direction of wind w.r.t. the “reference” direction

$|\bar{\omega}|$ - wind

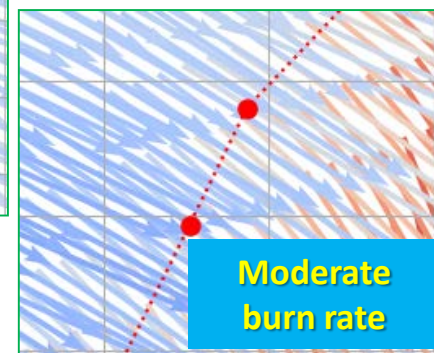
\bar{V}_g - ground speed



Strong headwind



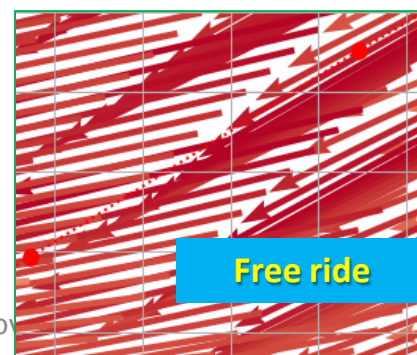
Moderate crosswind - sailing



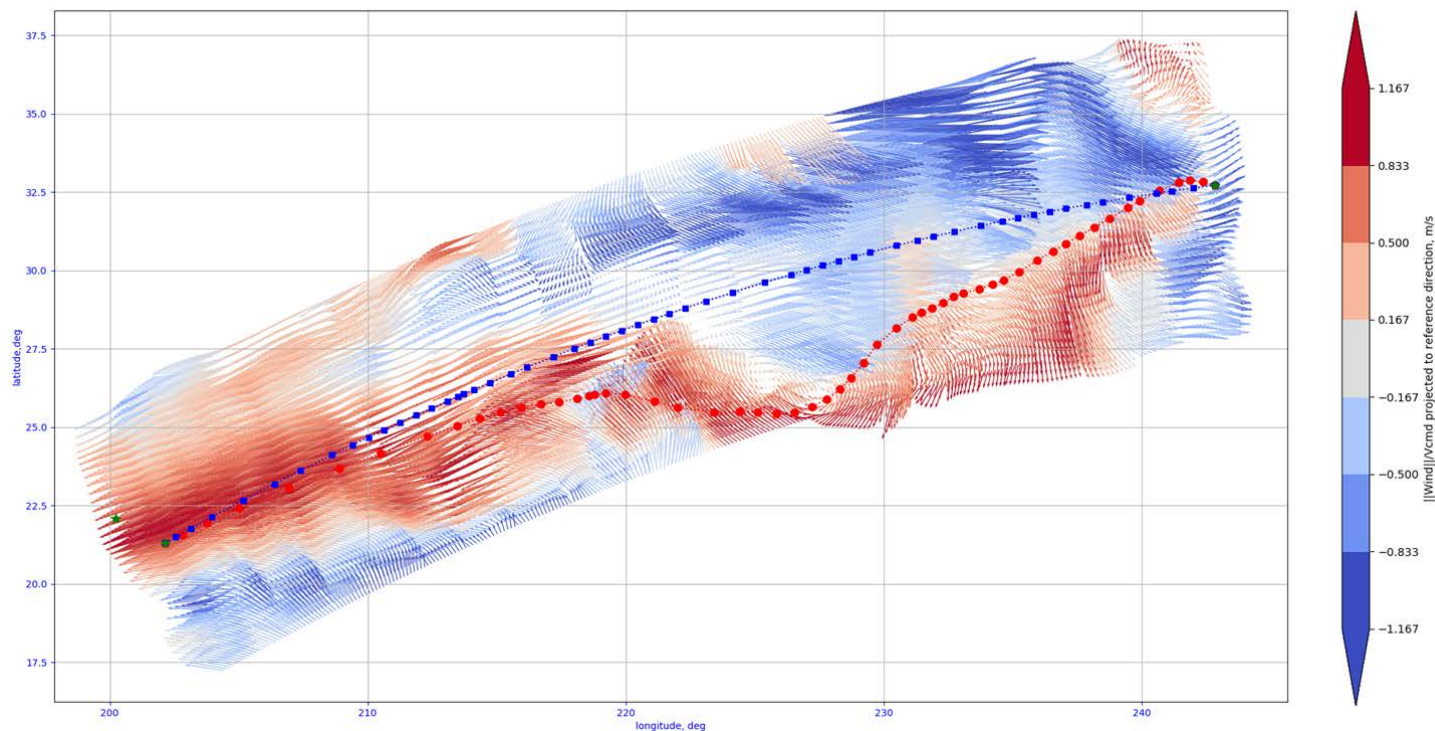
Moderate tailwind - sailing



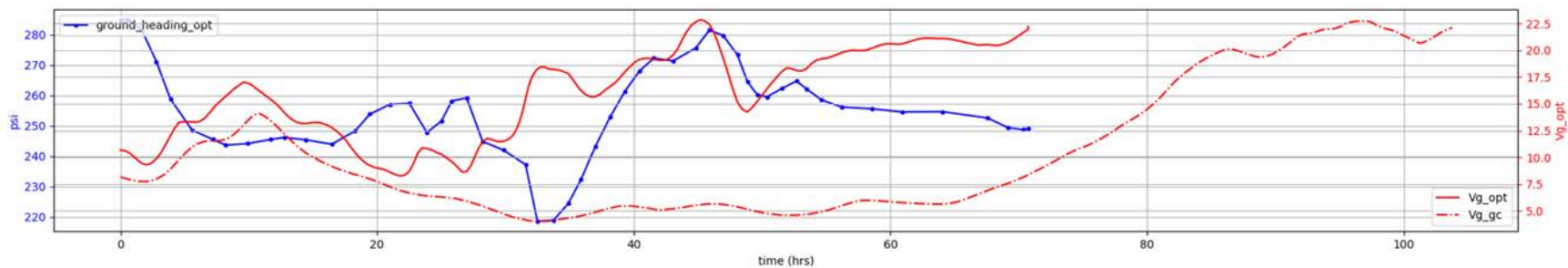
Strong tailwind



OC over Time-Varying COAMPS

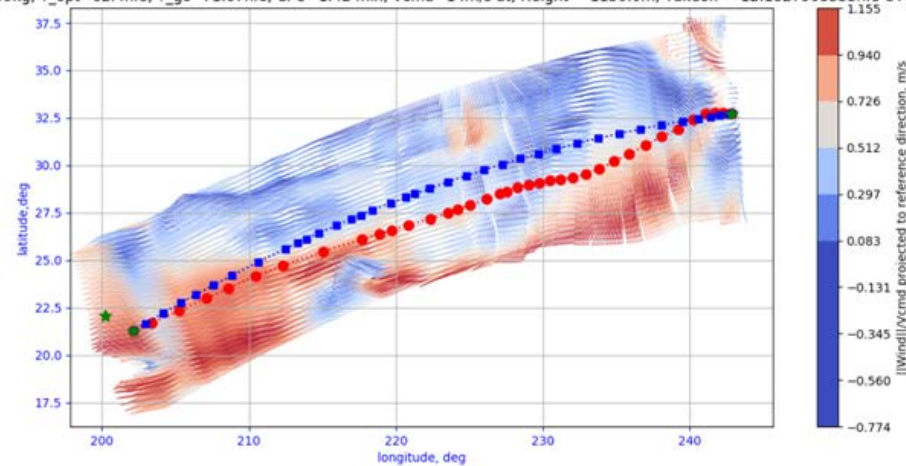
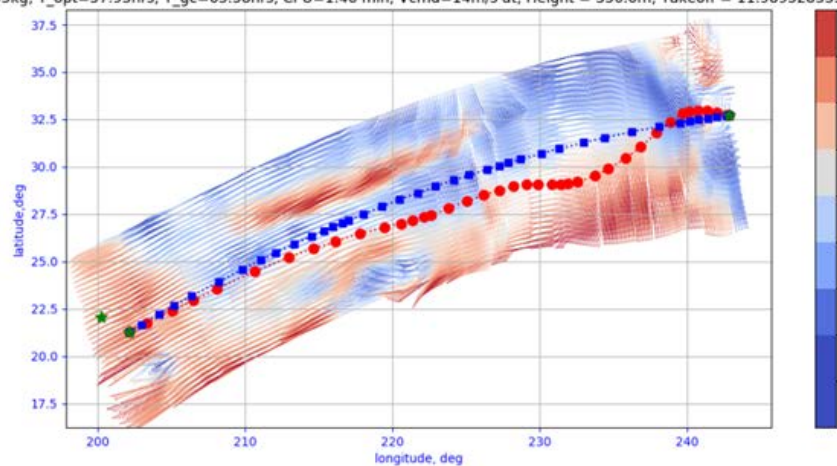


Comparison of the optimal and great circle routes/controls at H=2550 m

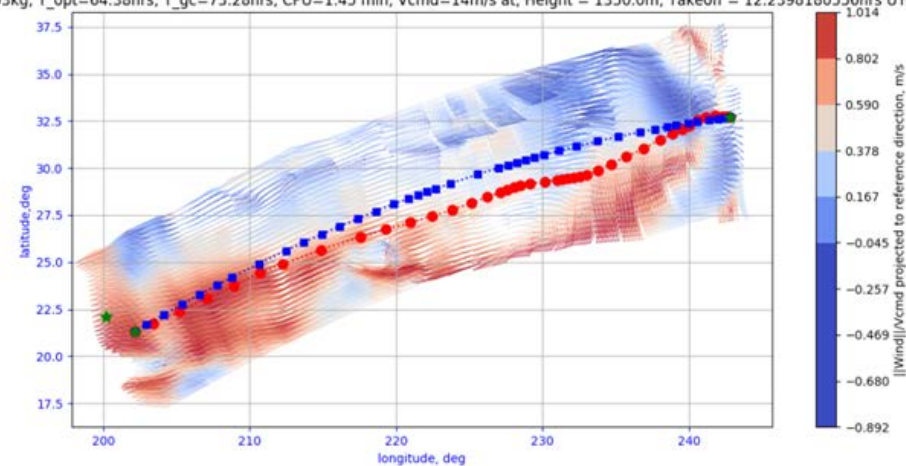
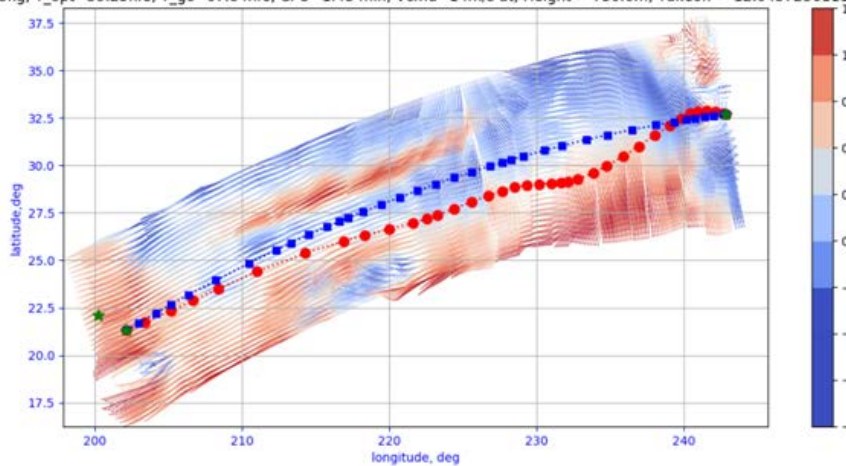


Robustness

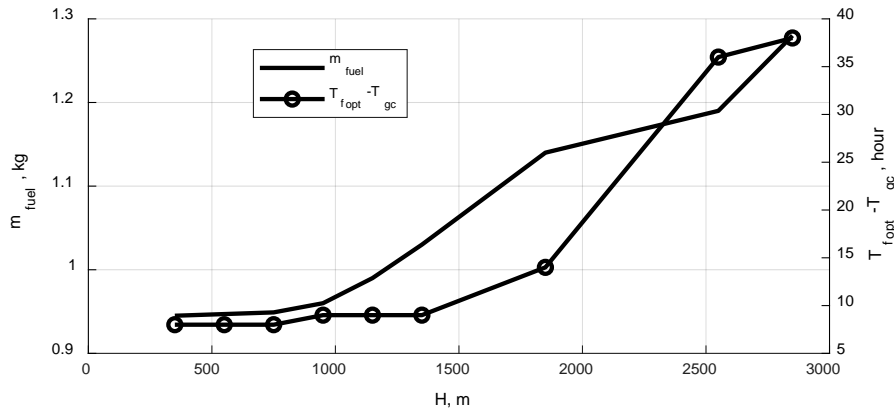
F_opt=0.95kg, T_opt=57.93hrs, T_gc=65.58hrs, CPU=1.46 min, Vcmd=14m/s at, Height = 350.0m, Takeoff = 11.989528333 F_opt=0.99kg, T_opt=62.4hrs, T_gc=71.67hrs, CPU=1.42 min, Vcmd=14m/s at, Height = 1150.0m, Takeoff = 12.182790833hrs UTC



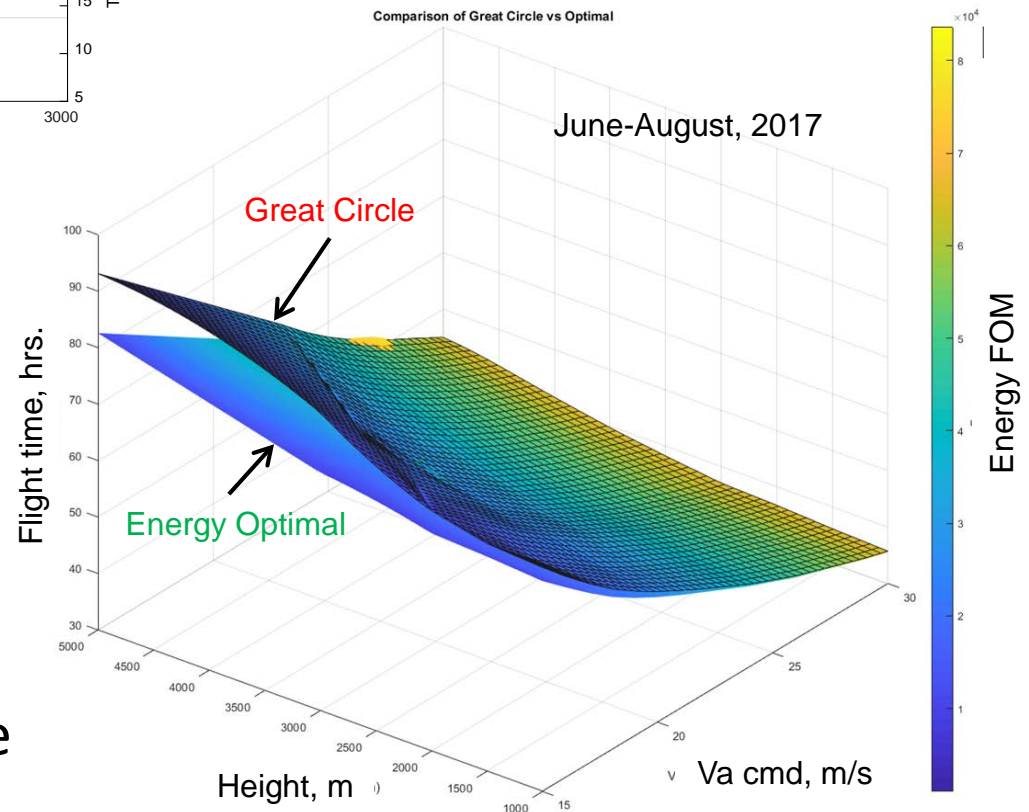
F_opt=0.95kg, T_opt=59.25hrs, T_gc=67.84hrs, CPU=1.43 min, Vcmd=14m/s at, Height = 750.0m, Takeoff = 12.045723611 F_opt=1.03kg, T_opt=64.38hrs, T_gc=73.28hrs, CPU=1.45 min, Vcmd=14m/s at, Height = 1350.0m, Takeoff = 12.239818055hrs UTC



Cumulative Results



- Va_{cmd} along GC matches the best airspeed for power
- Max achievable Time & Fuel benefits - up to ~11 hours or ~280g H_2
- It is really hard to compete with optimal control !!!

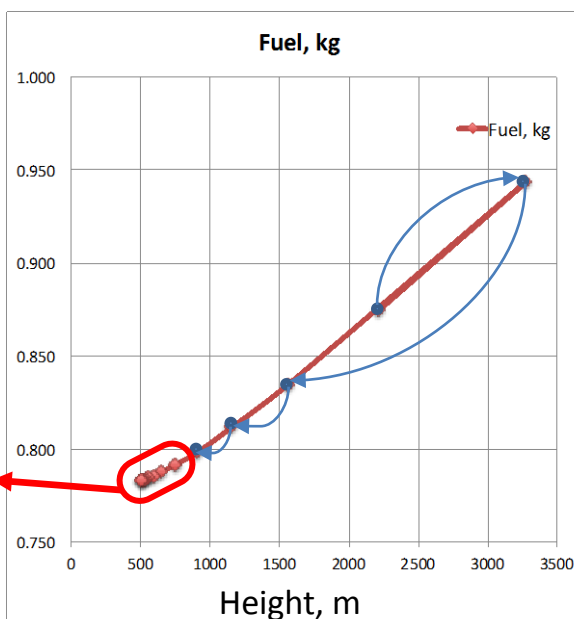




Questions ?

Log of Height Search with Fuel Tolerance = 10 gram (Ubuntu i7)

#	Height, m	Cost	Fuel, kg
1	2215.03	3148.08	0.874
2	3274.97	3396.22	0.943
3	1559.95	3003.83	0.834
4	1155.08	2921.9	0.812
5	904.863	2872.45	0.798
6	750.219	2849.51	0.792
7	654.644	2835.86	0.788
8	595.575	2827.79	0.785
9	559.069	2822.96	0.784
10	536.506	2820.9	0.784
11	522.562	2819.34	0.783
12	513.944	2818.03	0.783
13	508.618	2817.32	0.783
14	505.285	2817.11	0.783



It takes 8.25 min on i7(~times 5 in Odroid)
Can we afford or Do we want this higher
precision for the price of longer CPU time?

```

Wind scale = 1000.0 , Hcmd = 2215.02739051m
Iteration  Max residual  Total nodes  Nodes added
1          5.81e-01         10          18
...
7          4.10e-13        6562        (5920)
Wind scale = 100.0 , Hcmd = 2215.02739051m , P = [ 0.92444636]
Iteration  Max residual  Total nodes  Nodes added
...
3          1.79e-02         82         (162)
Wind scale = 10.0 , Hcmd = 2215.02739051m , P = [ 0.92027459]
Iteration  Max residual  Total nodes  Nodes added
...
3          1.44e-02         82         (162)
Wind scale = 1.0 , Hcmd = 2215.02739051m , P = [ 0.89845575]
Iteration  Max residual  Total nodes  Nodes added
...
3          9.27e-03         82         (162)
Number of nodes is exceeded after iteration 3, maximum relative residual 9.27e-03.

```

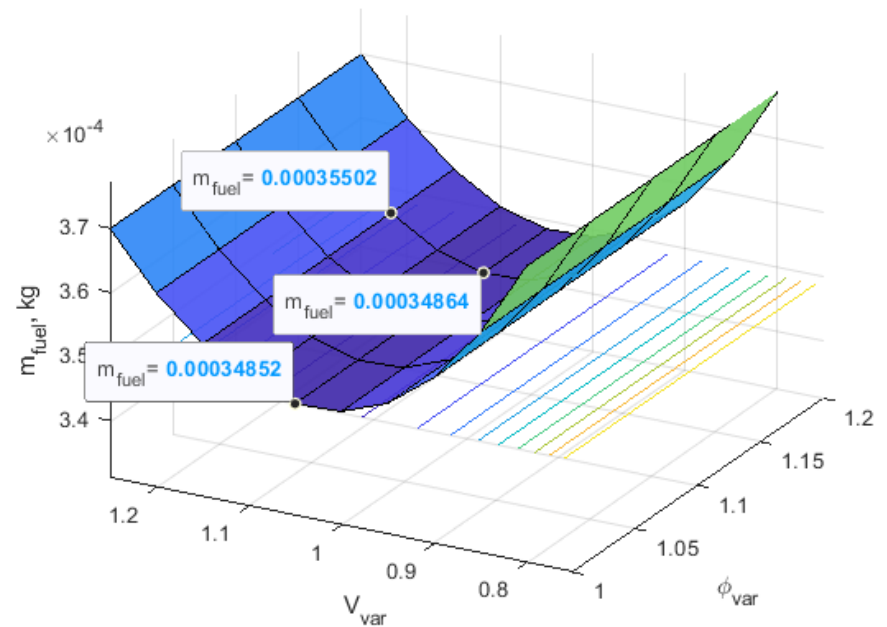
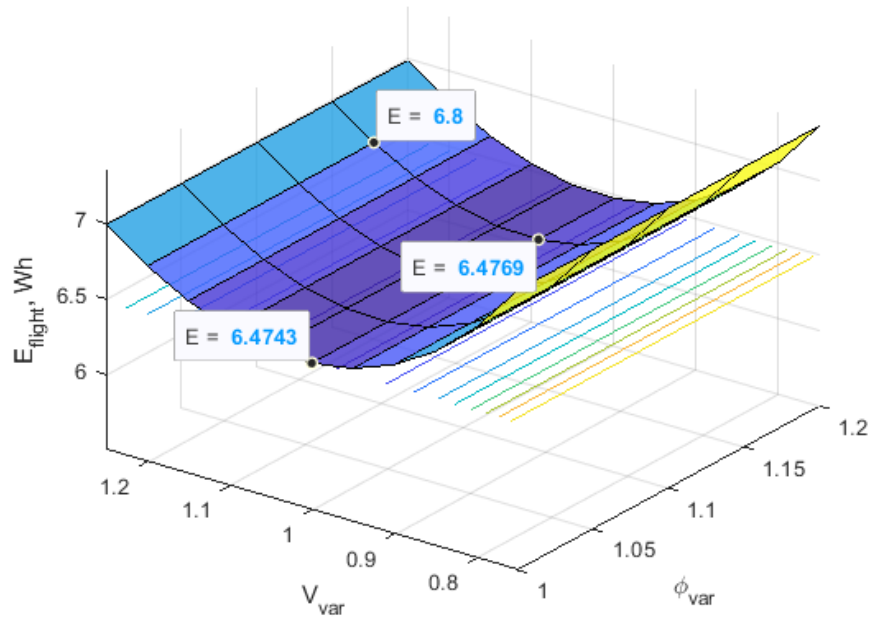
```

// Local search for best height
Func-count  x          f(x)          Procedure
1          2215.03      3148.08      initial
2          3274.97      3396.22      golden
3          1559.95      3003.83      golden
4          1155.08      2921.9       golden
5          904.863      2872.45      golden
6          750.219      2849.51      golden
7          654.644      2835.86      golden
8          595.575      2827.79      golden
9          559.069      2822.96      golden
10         536.506      2820.9       golden
11         522.562      2819.34      golden
12         513.944      2818.03      golden
13         508.618      2817.32      golden
14         505.285      2817.11      golden

Optimization terminated successfully;
The returned value satisfies the termination criteria
(using xtol : 10.0 )

```

Synthetic Wind :: Hessian



Road Map

