

Rotary Inverted Pendulum



The Quanser Rotary Inverted Pendulum consists of a flat arm, or hub, with a pivot at one end and a metal shaft on the other end. The pivot-end can be mounted on top of the SRV02 load gear shaft and fastened with screws. The actual pendulum link is fastened onto the metal shaft and the shaft is instrumented with a sensor to measure its angle. The result is a horizontally rotating arm with a pendulum at the end.

The student is challenged to apply the Euler-Lagrange equations to find the system equations of motion, followed by their linearization and state-space representation. This experiment supports studying and demonstrating both dynamic and static instability concepts and practices in control engineering (controllability, companion matrix, pole placement, feedback control, swing-up control).

Equations of motion

$$(m_p L_r^2 + \frac{1}{4} m_p L_p^2 - \frac{1}{4} m_p L_p^2 \cos(\alpha)^2 + J_r) \ddot{\theta} - \frac{1}{2} m_p L_p L_r \cos(\alpha) \ddot{\alpha} + \frac{1}{2} m_p L_p^2 \sin(\alpha) \cos(\alpha) \dot{\theta} \dot{\alpha} + \frac{1}{2} m_p L_p L_r \sin(\alpha) \dot{\alpha}^2 = \tau - B_r \dot{\theta}$$

$$-\frac{1}{2} m_p L_p L_r \cos(\alpha) \ddot{\theta} - (J_p + \frac{1}{4} m_p L_p^2) \ddot{\alpha} - \frac{1}{4} m_p L_p^2 \sin(\alpha) \cos(\alpha) \dot{\theta}^2 - \frac{1}{2} m_p L_p g \sin(\alpha) = B_p \dot{\alpha}$$

$$\tau = \frac{\eta_g K_g \eta_m k_t (V_m - K_g k_m \dot{\theta})}{R_m}$$

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}u$$

$$\mathbf{y} = \mathbf{C}\mathbf{x} + \mathbf{D}u$$

$$\mathbf{x} = \begin{bmatrix} \theta \\ \alpha \\ \dot{\theta} \\ \dot{\alpha} \end{bmatrix}$$

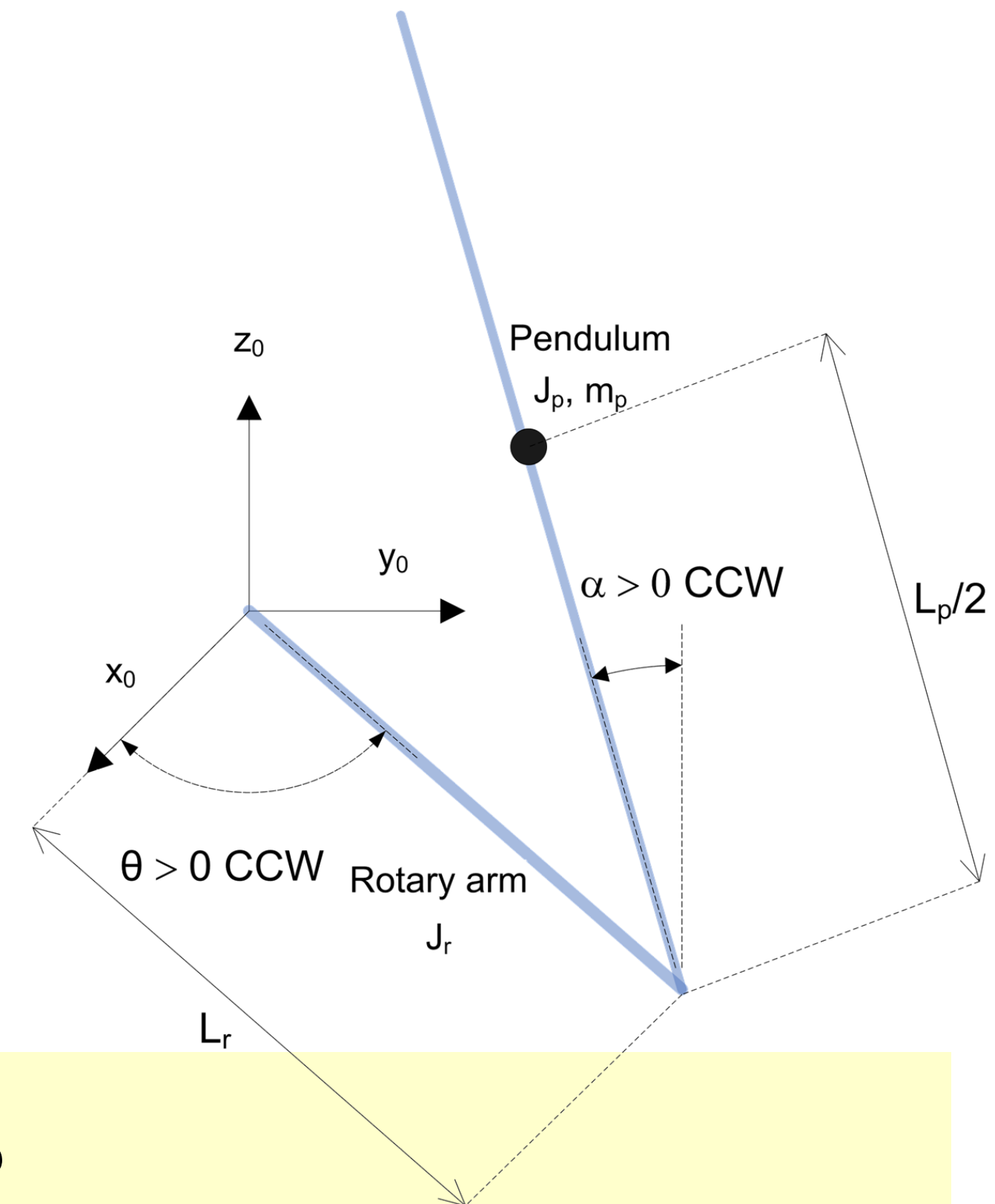
$$\mathbf{y} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\mathbf{A} = \frac{1}{J_r} \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ 0 & \frac{1}{4} m_p L_p^2 L_r g & -(J_p + \frac{1}{4} m_p L_p^2) B_r & -\frac{1}{2} m_p L_p L_r B_p \\ 0 & \frac{1}{2} m_p L_p g (J_r + m_p L_r^2) & \frac{1}{2} m_p L_p L_r B_r & (J_r + m_p L_r^2) B_p \end{bmatrix}$$

$$\mathbf{B} = \frac{1}{J_p m_p L_r^2 + J_r J_p + \frac{1}{4} J_r m_p L_p^2} \begin{bmatrix} 0 \\ 0 \\ J_p + \frac{1}{4} m_p L_p^2 \\ \frac{1}{4} m_p L_p L_r \end{bmatrix}$$

$$\mathbf{C} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}$$

$$\mathbf{D} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$



Specifications

Damping ratio:

$$\zeta = 0.7$$

Natural frequency:

$$\omega_n = 4 \text{ rad/s}$$

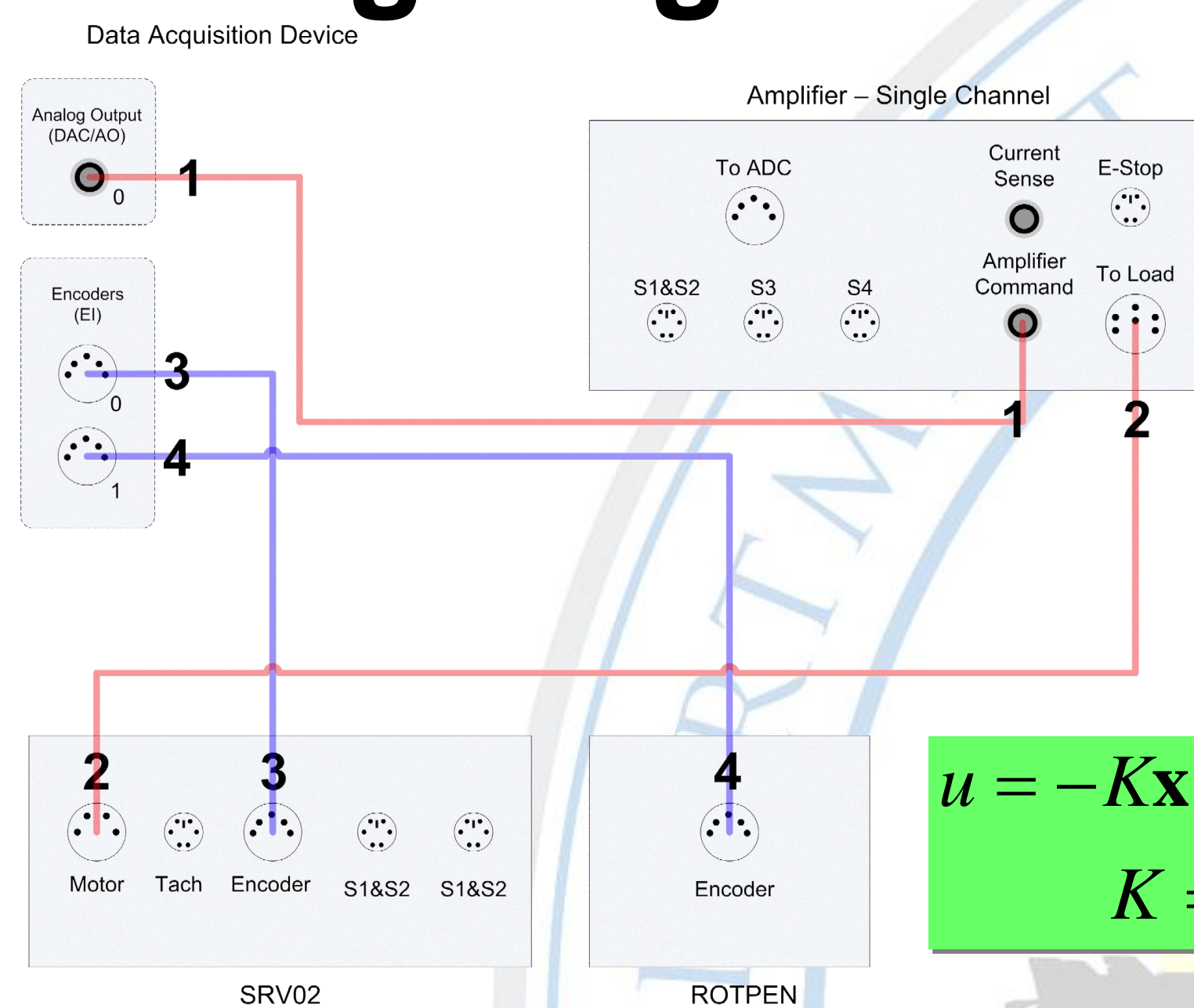
Maximum pendulum angle deflection:

$$|\alpha| < 15^\circ$$

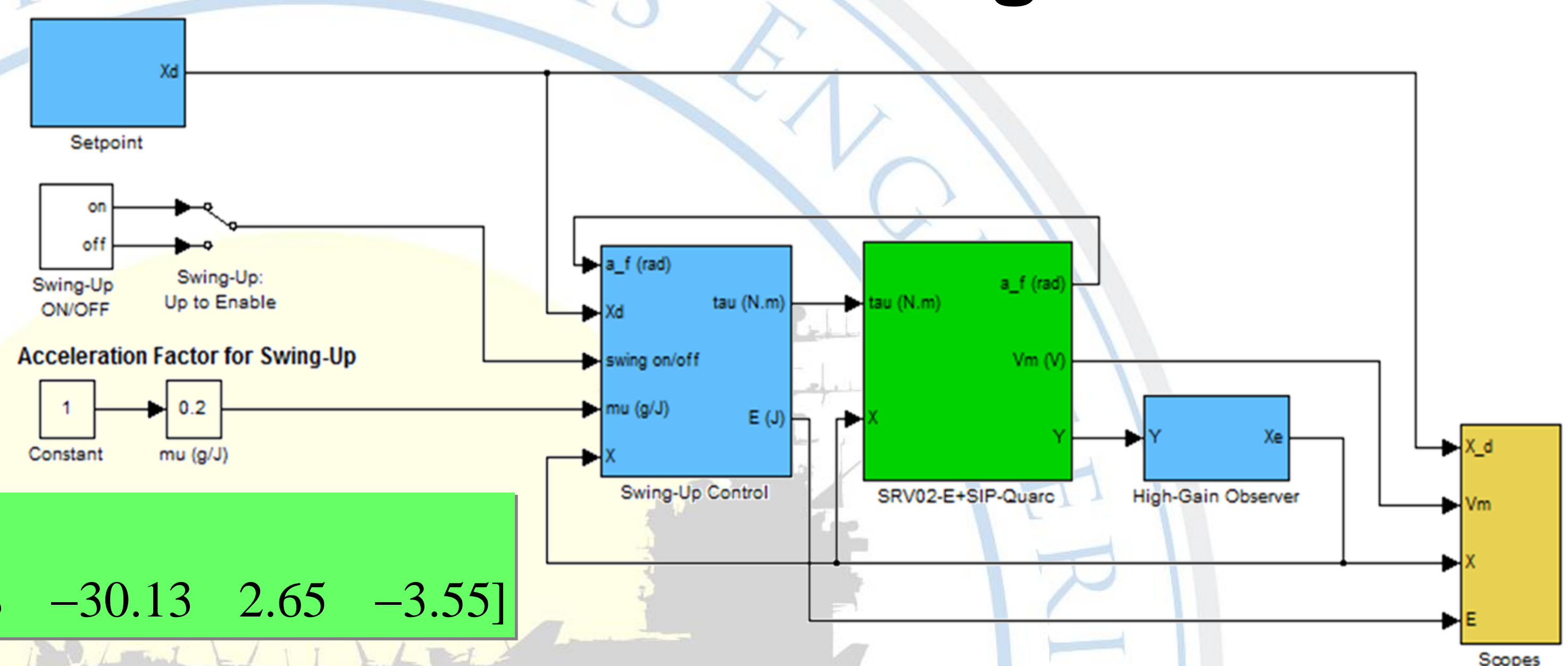
Maximum control effort / voltage:

$$|V_m| < 10 \text{ V}$$

Wiring diagram



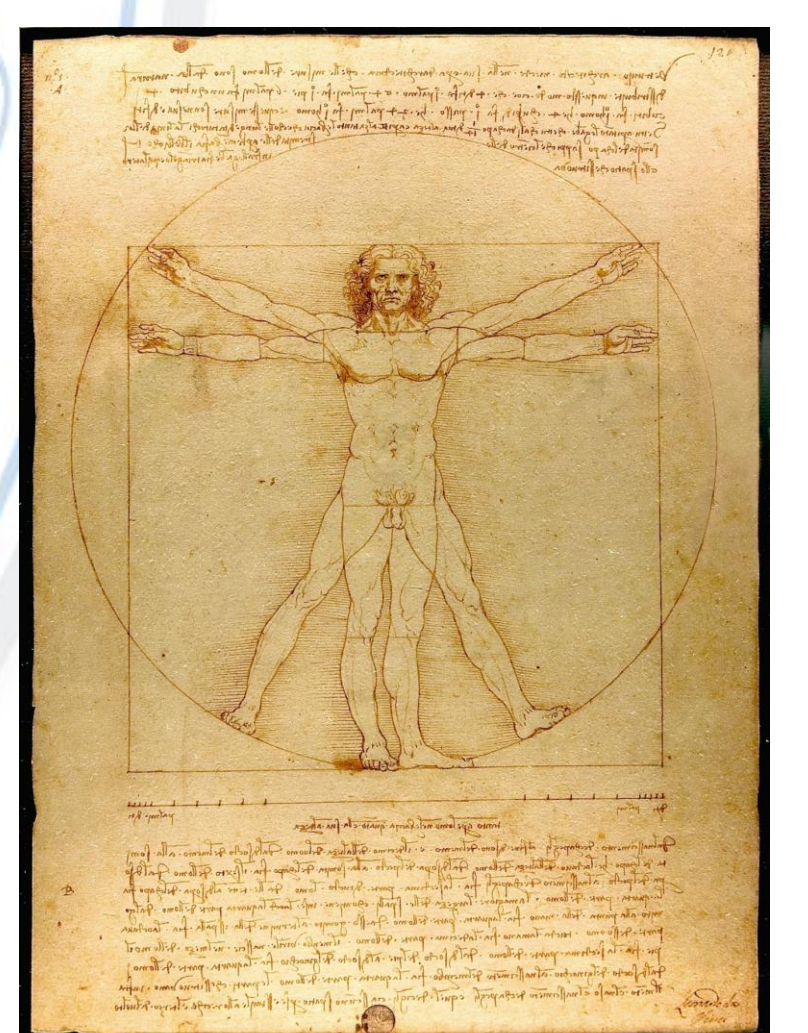
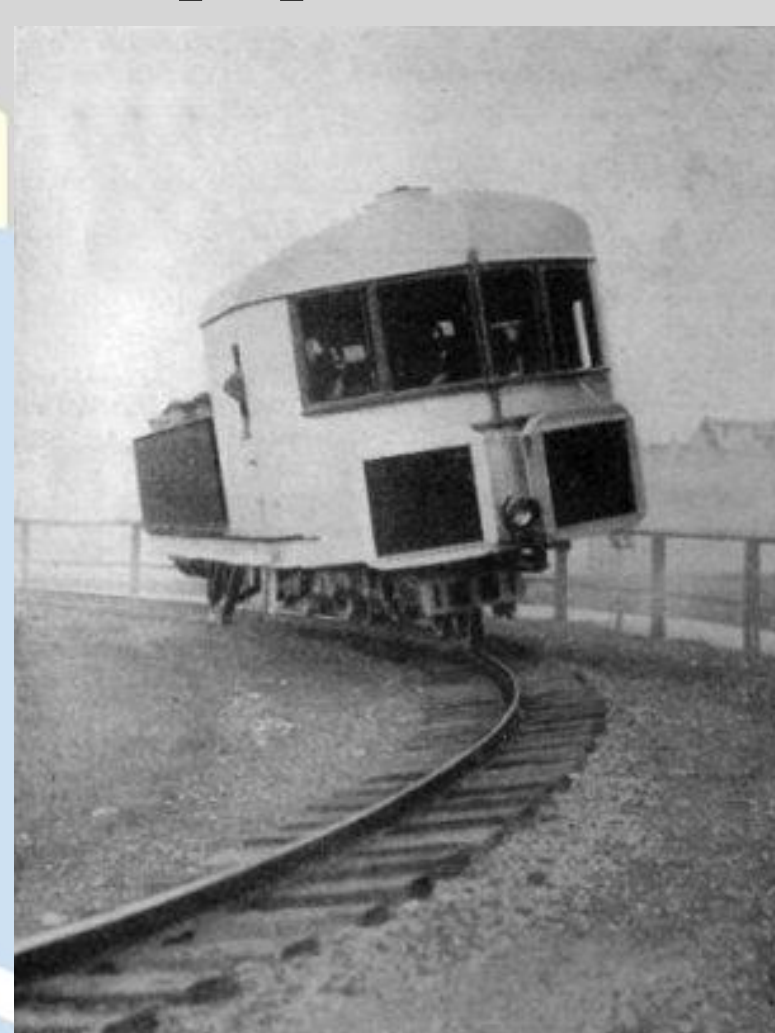
Simulink block diagram



$$u = -K\mathbf{x}$$

$$K = [5.28 \quad -30.13 \quad 2.65 \quad -3.55]$$

Applications



PoC: Prof. Oleg Yakimenko, Bu-223
oayakime@nps.edu, (831) 656-2826

